



## DINN360: Deformable Invertible Neural Network for Latitude-aware 360° Image Rescaling

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## Quick intro: 360° image rescaling



#### • Motivation and Contributions





#### **Contributions:**

- ① We find how the low-level characteristics of 360° images change along with its latitude, benefiting the designs of our method.
- 2 We propose a novel INN framework for 360° image rescaling, with the developed invertible deformable blocks to handle various spherical deformations.
- ③ We develop a latitude-aware conditional mechanism in our framework, to better preserve the high-frequency component of 360° images in a latitude-aware manner.

## Background



• Image rescaling:  $HR \rightarrow LR \rightarrow HR$ 



• **360** • **Images:** an omnidirectional view



Non-uniform mapping



Equiangular projection (ERP)





• Finding 1: In 360° images, low-latitude regions tend to contain more textures, leading to larger HF components.



• Finding 2: In 360° images, the larger HF components at low-latitude regions result in worse rescaling performance for the existing 2D rescaling methods.



Analysis





## Method



• Pipeline of DINN360



- (1) Deformable downscaling  $\hat{\mathbf{x}} \rightarrow [\mathbf{y}; \mathbf{h}]$ : downscales the HR image  $\hat{\mathbf{x}}$  into LR image  $\mathbf{y}$  and HF component  $\mathbf{h}$  by invertible deformable (ID) blocks.
- (2) Latitude-aware HF projection [y; h] → z: projects the split HF component h into latent variable z, which is conditional on LR image y.
- (3) Reverse upscaling [y; ž] → x: recovers the HF component h and upscales the LR image into reconstructed HR image x by reversely passing stage (1) and stage (2).

## Method



• Deformable Swin Transformer (DST) Module



(a) Affine functions in ID block: The functions are built in a deformable manner, upon the residual structure with deformable convolution (DConv) layers and the developed deformable swin transformer (DST) modules.

(b) Deformable swin transformer module: The referenced sampling points are scaled and shifted into deformed points by the scale head and offset head, which is used to produce the deformable token **q**.

## Method



#### • Backflow training protocol

**Algorithm 1:** Training process for 2× rescaling. **Input:** HR image  $\hat{\mathbf{x}}$ , LR image  $\hat{\mathbf{y}}$  and distortion map  $\hat{\mathbf{c}}^{lat}$ . **Output:** Trained  $I_{\rm D}(\cdot) I_{\rm P}(\cdot)$  and  $G_{\rm SC}(\cdot)$ . **Variables:** Training variables  $\Phi$ , latent variables  $\mathbf{z}, \mathbf{\tilde{z}}$ . **Parameters:**  $\lambda_{\rm H}, \lambda_{\rm L}, \lambda_{\rm z}, \alpha$  and learning rate lr. Initialize  $\Phi$  with Gaussian initialization. 2 while Step < max steps do  $\mathbf{y}, \mathbf{h} = I_{\mathrm{D}}(\hat{\mathbf{x}}).$ 3  $\mathbf{c} = [\mathbf{c}^{\mathrm{con}}, \mathbf{c}^{\mathrm{lat}}] = G_{\mathrm{SC}}(\mathbf{y}).$ 4 if Step < backflow steps then 5  $\widetilde{\mathbf{h}} = I_{\mathbf{P}}^{-1}(\widetilde{\mathbf{z}}, \mathbf{c}).$ 6  $\mathbf{h} = \alpha \widetilde{\mathbf{h}} + (1 - \alpha)\mathbf{h}.$ 7 8 end  $\mathbf{z} = I_{\mathrm{D}}(\mathbf{h}, \mathbf{c}).$ 9  $\widetilde{\mathbf{h}} = I_{\mathbf{P}}^{-1}(\widetilde{\mathbf{z}}, \mathbf{c}).$ 10  $\begin{aligned} \mathbf{x} &= I_{\mathrm{D}}^{-1}(\mathbf{y}, \widetilde{\mathbf{h}}). \\ \mathcal{L} &= \lambda_{\mathrm{H}} \ell_1(\mathbf{x}, \hat{\mathbf{x}}) + \lambda_{\mathrm{L}} \ell_2(\mathbf{y}, \hat{\mathbf{y}}) + \lambda_{\mathbf{z}} \ell_2(\mathbf{z}, \widetilde{\mathbf{z}}). \\ \Phi &\leftarrow \Phi - lr \cdot \nabla_{\Phi} \mathcal{L}. \end{aligned}$ 11 12 13 end 14 return  $\Phi$ .



#### For better training INN:

- (1) Inspired by the proportional feedback in PID control;
- (2) Regarding the forward and reverse model together as an invertible system;
- (3) Minimize the gap between the generated and sampled latent variable.





#### • Quantitative results

Scale	Method	ODISR [4]	SUN360 [38]	F-360iSOD [42]	YouTube360 [27]	
	Bicubic	$29.46 \pm 2.54$ / $86.23 \pm 5.05$	$30.06 \pm 2.46$ / $87.92 \pm 4.85$	$30.68 \pm 4.53$ / $87.43 \pm 7.23$	$34.93 \pm 4.92$ / $94.82 \pm 4.47$	
2×	Bilinear	$28.94 \pm 2.45$ / $83.15 \pm 5.83$	$29.39 \pm 2.40$ / $85.09 \pm 6.08$	$29.97 \pm 4.23$ / $84.61 \pm 8.61$	$33.20 \pm 4.21  /  9.255 \pm 6.06$	
	Lanczos	$28.58 \pm 2.54$ / $84.04 \pm 5.57$	$29.16 \pm 2.47$ / $85.72 \pm 5.48$	$29.86 \pm 4.56$ / $85.44 \pm 8.11$	$34.26 \pm 5.13$ / $93.95 \pm 5.24$	
	Bicubic & 360SR [28]	$27.05 \pm 2.36$ / $80.46 \pm 4.32$	$27.69 \pm 2.20$ / $81.55 \pm 4.87$	$26.08 \pm 4.17$ / $78.08 \pm 5.39$	$32.12 \pm 3.77$ / $89.84 \pm 4.85$	
	Bicubic & 360SISR [27]	$30.81 \pm 2.90$ / $87.44 \pm 5.17$	$32.72 \pm 2.79  /  90.53 \pm 5.10$	$31.33 \pm 4.81$ / $89.63 \pm 6.28$	$37.62 \pm 5.21  /  96.23 \pm 5.08$	+0.19~0.67dF
	TAD & TAU [16]	$35.84 \pm 3.28$ / 96.12 $\pm$ 8.12	$37.70 \pm 2.68$ / $97.17 \pm 1.10$	$33.94 \pm 5.11$ / $93.87 \pm 4.47$	$39.50 \pm 4.08$ / $98.22 \pm 1.00$	
	CAR & EDSR [22, 32]	$33.00 \pm 3.51  /  91.31 \pm 4.41$	$35.68 \pm 3.37$ / $93.91 \pm 4.07$	$35.38 \pm 5.48$ / $93.05 \pm 5.09$	$40.49 \pm 5.24$ / $97.75 \pm 2.55$	
	IRN [39]	$40.51 \pm 3.52  /  98.63 \pm 0.71$	$42.72 \pm 2.73  /  99.11 \pm 0.32$	$39.83 \pm 5.74$ / $97.83 \pm 2.05$	$46.15 \pm 4.02  /  99.50 \pm 0.32$	
	HCFlow [21]	$42.05 \pm 3.79  /  99.02 \pm 0.57$	$45.05 \pm 3.00 / 99.49 \pm 0.24$	$\underline{40.53 \pm 5.78  /  97.92 \pm 1.99}$	$50.56 \pm 3.07 / 99.71 \pm 0.10$	
	DINN360	$42.64 \pm 3.87  /  99.13 \pm 0.52$	$45.72 \pm 3.00/99.56 \pm 0.21$	$40.77 \pm 5.88  /  97.93 \pm 2.21$	$50.75 \pm 3.07  /  99.73 \pm 0.10$	
	Bicubic	$25.39 \pm 2.28$ / $72.27 \pm 7.45$	$25.38 \pm 2.33$ / 73.75 $\pm$ 8.83	$26.16 \pm 3.91 / 73.75 \pm 12.38$	$28.29 \pm 3.80 / 83.73 \pm 10.58$	
	Bilinear	$26.24 \pm 2.27$ / $72.96 \pm 7.54$	$26.22 \pm 2.29$ / 74.72 $\pm$ 8.85	$26.85 \pm 3.78$ / 74.30 $\pm$ 12.38	$28.92 \pm 3.53 / 83.94 \pm 10.44$	
	Lanczos	$24.97 \pm 2.28$ / 70.69 $\pm$ 7.64	$24.99 \pm 2.33  /  71.95 \pm 9.05$	$25.77 \pm 3.94$ / $72.10 \pm 12.84$	$27.97 \pm 3.85$ / $82.65 \pm 11.02$	
	Bicubic & 360SR	$25.42 \pm 2.26$ / 71.06 $\pm$ 6.89	$25.42 \pm 2.16$ / 72.46 $\pm$ 8.64	$25.19 \pm 3.69$ / 70.79 $\pm$ 9.83	$28.43 \pm 3.26$ / $83.06 \pm 9.36$	
4.4	Bicubic & 360SISR	$27.03 \pm 2.45$ / 76.15 $\pm$ 7.97	$27.81 \pm 2.44$ / $80.45 \pm 9.39$	$27.45 \pm 4.35$ / 78.79 $\pm$ 11.66	$30.96 \pm 3.87$ / $89.36 \pm 10.75$	10 24 0 57 11
4×	TAD & TAU	$28.98 \pm 2.51$ / $82.69 \pm 5.91$	$29.70 \pm 2.47$ / $84.86 \pm 6.21$	$28.71 \pm 4.55$ / $81.34 \pm 10.40$	$33.24 \pm 4.61$ / $92.48 \pm 6.08$	+0.24~0.5/01
	CAR & EDSR	$29.61 \pm 2.86$ / $82.82 \pm 6.76$	$31.32 \pm 2.82$ / $86.60 \pm 7.49$	$31.33 \pm 4.94$ / $85.30 \pm 9.10$	$34.85 \pm 4.69$ / $93.08 \pm 6.45$	
	IRN	$30.86 \pm 3.06$ / $87.47 \pm 5.56$	$32.69 \pm 2.92$ / $90.41 \pm 5.41$	$32.58 \pm 5.19$ / $88.95 \pm 7.29$	$36.85 \pm 4.78$ / $95.86 \pm 4.07$	
	HCFlow	$31.48 \pm 3.16 / 89.07 \pm 5.02$	$33.62 \pm 3.03  /  92.00 \pm 4.78$	$32.40 \pm 5.79$ / $88.44 \pm 8.85$	$40.31 \pm 4.44  /  97.72 \pm 2.13$	
	DINN360	$31.92 \pm 3.26  /  89.90 \pm 4.82$	$34.19 \pm 3.12  /  92.77 \pm 4.48$	$32.93 \pm 5.90$ / $89.34 \pm 8.82$	$40.55 \pm 4.29/97.89 \pm 1.89$	
	Bicubic	$23.25 \pm 2.19$ / 64.10 $\pm$ 8.64	$22.92 \pm 2.21$ / $65.18 \pm 10.24$	$23.45 \pm 3.48$ / $64.12 \pm 15.04$	$24.98 \pm 3.06$ / 74.70 $\pm$ 12.89	
	Bilinear	$24.16 \pm 2.19$ / $65.35 \pm 8.65$	$23.81 \pm 2.19$ / 66.77 $\pm$ 10.20	$24.25 \pm 3.41$ / $65.42 \pm 14.89$	$25.78 \pm 2.96$ / $75.86 \pm 12.65$	
	Lanczos	$22.95 \pm 2.19$ / $63.15 \pm 8.68$	$22.65 \pm 2.21$ / $63.98 \pm 10.27$	$23.19 \pm 3.49$ / $63.05 \pm 15.18$	$24.77 \pm 3.08$ / 73.78 $\pm$ 13.03	
	Bicubic & 360SR	$23.61 \pm 2.06$ / $64.15 \pm 8.53$	$23.28 \pm 2.17$ / $65.11 \pm 10.14$	$23.19 \pm 3.17$ / $63.30 \pm 13.68$	$25.02 \pm 2.85$ / 78.19 $\pm$ 12.37	
	Bicubic & 360SISR	$24.63 \pm 2.26$ / $67.75 \pm 8.99$	$24.56 \pm 2.27$ / $70.80 \pm 10.66$	$24.53 \pm 3.62$ / $68.64 \pm 14.76$	$26.28 \pm 3.01/80.02 \pm 12.73$	
$8 \times$	Bicubic & LAU-Net [4]	$24.37 \pm 2.22$ / $66.64 \pm 8.83$	$24.21 \pm 2.26$ / 69.37 $\pm$ 10.63	$24.18 \pm 3.57$ / $66.94 \pm 14.99$	$25.81 \pm 2.94$ / 77.33 $\pm$ 12.61	+0.35~0.74dI
	TAD & TAU	$26.36 \pm 2.30  /  71.36 \pm 7.86$	$26.50 \pm 2.33 / 73.43 \pm 9.36$	$25.94 \pm 4.10  /  70.35 \pm 14.15$	$28.36 \pm 3.46  /  81.61 \pm 11.04$	
	CAR & EDSR	$25.97 \pm 2.38$ / 69.40 $\pm$ 8.82	$26.40 \pm 2.42$ / $72.77 \pm 10.75$	$26.87 \pm 4.12 / 71.19 \pm 14.36$	$27.98 \pm 3.44$ / 79.83 $\pm$ 11.27	
	IRN	$28.06 \pm 2.72  /  77.41 \pm 8.12$	$29.48 \pm 2.74$ / $82.02 \pm 9.66$	$29.55 \pm 4.89$ / $80.03 \pm 11.87$	$32.16 \pm 4.24$ / $89.01 \pm 9.30$	1
	HCFlow	$\underline{28.25 \pm 2.76  /  78.20 \pm 8.00}$	$\underline{29.77 \pm 2.77  /  82.84 \pm 9.42}$	$29.83 \pm 4.94$ / $80.98 \pm 11.47$	$\underline{34.19 \pm 4.02  /  91.78 \pm 7.14}$	
	DINN360	$28.60 \pm 2.86  \textit{/}  79.17 \pm 7.98$	$30.36 \pm 2.87$ / $84.02 \pm 9.36$	$30.29 \pm 5.13  /  82.07 \pm 11.22$	$34.93 \pm 4.17$ / $92.58 \pm 6.83$	





• Qualitative results







• Qualitative results



### Experiments



#### • Ablation results



	Ablation settings	WS-PSNR	WS-SSIM
ID block	w/o DST module	$31.79 \pm 3.14$	$89.68 \pm 4.17$
ID DIOCK	w/o deform	$31.83\pm3.63$	$89.75\pm4.29$
ID block	w/o latitude head	$31.85 \pm 3.21$	$89.74 \pm 4.31$
IF DIOCK	w/o content head	$31.76 \pm 3.21$	$89.56 \pm 4.08$
backflow	w/o feedback	$31.85 \pm 3.32$	$89.83 \pm 4.27$
-	DINN360	$31.92 \pm 3.26$	$\textbf{89.90} \pm \textbf{4.82}$

#### Hyper-parameter values:

- (1) Number of ID/IP blocks;
- (2) Feedback ratio of backflow training protocol

#### Ablation studies:

- (1) ID/IP block: deformable and latitude-aware
- (2) Backflow: feedback protocol





# Thanks



#### **Contact us**

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